

Appendix A: Coldwater Pool Diversion Analysis (EID 2009)



United States Department of the Interior

BUREAU OF RECLAMATION
Mid-Pacific Region
Central California Area Office
7794 Folsom Dam Road
Folsom, CA 95630-1799

FEB 01 2011

IN REPLY REFER TO:

CC-608A
PRJ-4.00

ORIGINAL IN FILE

Mr. Bob Rice
Senior Engineer
El Dorado Irrigation District
2890 Mosquito Road
Placerville, California 95667

Subject: Lowest Intake Revision Recommendation, Folsom Lake Intake and Pump Station
El Dorado Irrigation District (EID) Project No. 04003E.02

Dear Mr. Rice:

Thank you for your letter dated December 17, 2010, which proposes to raise the lowest water intake for the EID Temperature Control Device from elevation 320 to 325 feet mean sea level. We have reviewed the Folsom Lake Temperature Model iterations created by the contractor, HDR, Inc., other supporting information, and discussed the foreseeable impacts to the Folsom Lake cold water pool.

On October 16, 2009 the Bureau of Reclamation approved EID's proposed intake elevations at 320, 370, and 410 feet mean sea level.

Reclamation concurs with the change of the lowest intake from 320 to 325 feet mean sea level which should have no adverse impact on the preservation of the Folsom Lake cold water pool. Reclamation also wants to reiterate the two points made in our October 2009 letter:

1. Taking water from the lowest intake should be minimized as much as possible.
2. Temperature Control Device operation logs should be made available to Reclamation.

Please direct any questions to Mr. Peter Funkhouser at 916-989-7161 or pfunkhouser@usbr.gov.

Sincerely,

Michael R. Finnegan
Area Manager

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FEB 03 2011

ADMINISTRATIVE
SERVICES

cc: See next page.

cc: Mr. Thomas D. Cumpston
El Dorado Irrigation District
2890 Mosquito Road
Placerville, California 95667



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OCT 16 2009

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OCT 20 2009

ADMINISTRATIVE
SERVICES

Mr. Thomas D. Cumpston
General Counsel/Interim General Manager
El Dorado Irrigation District
2890 Mosquito Road
Placerville, California 95667

Subject: Final Cold Water Pool Diversion Analysis, Folsom Lake Temperature Control Device

Dear Mr. Cumpston:

In response to your transmittal letter dated August 18, 2009, we have reviewed the El Dorado Irrigation District's Folsom Lake Cold Water Pool Diversion Analysis report.

The report concludes that three intakes are most practical and the elevations of the proposed intakes; 320, 370, and 410 feet mean sea level will reduce withdrawals from the cold water pool. The Bureau of Reclamation concurs with these conclusions and general design concept with the following comments:

1. Taking water from the 320 feet intake should be minimized as much as possible.
2. Temperature Control Device operation logs should be made available to Reclamation.

Please direct any questions to Peter Funkhouser at 916-989-7161 or pfunkhouser@usbr.gov.

Sincerely,

Michael R. Finnegan
Area Manager

cc: Mr Bob Rice
El Dorado Irrigation District
2890 Mosquito Road
Placerville, California 95667

George A. Wheeldon – *President*
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El Dorado Irrigation District

John P. Fraser – *Vice President*
Division 2

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Division 5

Thomas D. Cumpston
General Counsel/
Interim General Manager

In Reply Refer To: M0809-066 and EOL0809-196

August 18, 2009

Michael Finnegan
Area Manager, Central California Area Office
U.S. Bureau of Reclamation
7794 Folsom Dam Road
Folsom, CA 95630-1799

Subject: Final Cold Water Pool Diversion Analysis, Folsom Lake Temperature Control Device

M J.
Dear Mr. Finnegan:

The El Dorado Irrigation District (EID) is pleased to submit the enclosed final temperature model and summary results for the Folsom Lake cold water pool diversion analysis. The model was created to assist EID in designing the new Folsom Lake Temperature Control Device (TCD) consistent with U.S. Bureau of Reclamation (Reclamation) Cooperative Agreement 05FC2011041 (Agreement), which states that the TCD would allow for EID to preserve more of the cold water pool for downstream Reclamation needs.

As specified by subtasks 1A and 2A of the Agreement, EID has completed this analysis as a screening study to determine the overall management, administrative, and environmental liability and economic attractiveness of different design concepts without pursuing the concepts in great detail. The documentation included with this screening study are a summary of the modeling analysis, model output tables, full VBA macro Microsoft Excel model (via CD), and a tutorial that will assist Reclamation's review of the model.

EID is seeking Reclamation's concurrence with the three-intake design concept outlined below, so that EID may complete design of the temperature control component of EID's new Folsom Lake intake. Because EID has identified this screening study as a critical path in the design process, we request Reclamation's concurrence on this design concept by September 18, 2009.

The enclosed submittals are the fruit of an extended collaborative effort. Over the past year, staff from our respective agencies have been working together to develop the enclosed model as a tool for designing the temperature control device component of EID's

new Folsom Lake intake. Based upon the recommendations of Reclamation staff, this final version of the model incorporates the following revisions to assist in its evaluation:

1. The ability to vary the target temperature between 60°F and 64°F to model Reclamation's downstream temperature targets at Watt Avenue.
2. Presentation of diversion data in both acre-feet and as a percentage of volume to evaluate benefits of each alternative configuration.
3. Results for each calendar year (2002 through 2008) based on lake level and temperature conditions for demands ranging from existing demand to projected years 2013 and 2030 demands.

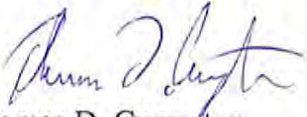
To assist with Reclamation review of the model findings, EID has enclosed summary figures generated by the model output to illustrate the results and support our recommendations for the number and elevation of the intakes. Figures 1 through 7 illustrate the intake elevations as optimized by the model, for individual calendar years 2002 through 2008. Each figure represents one specific calendar year, and each year's results illustrate six alternatives of various numbers of intakes. These figures allow direct side-by-side comparison of the cumulative benefit resulting from the sequential addition of intakes. Figure 8 provides the final best average configuration based on temperature and lake level conditions throughout the entire period of 2002 through 2008. Also provided with this transmittal are Tables 1 through 12 generated by the model, which include the detailed data utilized to generate the above listed figures. Each pair of tables provides results in tabular form for a given demand flow (existing, and years 2013 and 2030), given minimum head required over the intake screen, (10 ft or 15 ft), and diversion results in either acre-feet or percent.

These figures demonstrate significant benefits to Reclamation's maintenance of the cold water pool over existing conditions when the low-water intake is supplemented by one and two temperature control intakes. However, any additional temperature control intakes provide negligible benefits to the cold water pool while representing significant additional capital and operations and maintenance costs to EID.

Based on review of the final model results, EID is requesting Reclamation's concurrence that intakes at 320 feet (ft) mean sea level (MSL), 370 ft MSL, and 410 ft MSL operating at a minimum depth of 15 ft will fulfill the Agreement by minimizing withdrawals from the cold water pool while allowing EID to maintain a reliable diversion of water from Folsom Lake. Again, Reclamation's concurrence with a total of three intakes is necessary before EID can proceed with the design phase. To maintain our schedule, we are requesting that concurrence no later than September 18.

We thank you for the assistance of your staff in developing this tool and look forward to your concurrence. If there are any questions regarding the analysis, please contact Bob Rice, EID Senior Engineer at (530) 642-4079 or brice@eid.org.

Sincerely,



Thomas D. Cumpston
General Counsel/Interim General Manager

TC/BR:ss

Enclosures:

- Technical Memorandum: Cold Water Pool Diversion Analysis for Folsom Lake Raw Water Pump Station
- Addendum: Temperature Control Device Model Tutorial
- Figures 1 through 8: Best Annual and Average Configuration 2002-2008
- Tables 1 through 12: Comparison of Alternative Intake Configurations under Existing, 2013, and 2030 Projected Demands
- Temperature Model Program (2 CD's to Peter Funkhouser only)

cc w/enclosures:

Dan Netto, Reclamation
Peter Funkhouser, Reclamation
Robert Schroeder, Reclamation

El Dorado Irrigation District:

Brian Mueller, Director of Engineering
David Witter, Director of Natural Resources
Dan Corcoran, Environmental Manager
Bob Rice, Senior Civil Engineer

Cold Water Pool Diversion Analysis

For

El Dorado Irrigation District

Folsom Lake Raw Water Pump Station

Executive Summary

Folsom Lake is operated by the United States Bureau of Reclamation (Reclamation) as part of the Central Valley Project (CVP) to provide water for irrigation, municipal and industrial uses, hydroelectric power, recreation, water quality, flood control, and fish protection. One of Reclamation's operational goals at Folsom Lake is to manage the temperature of the water releases from Folsom Lake for the benefit of the downstream aquatic resources in the lower American River (LAR). This goal requires careful management by Reclamation of the available Cold Water Pool (CWP) in Folsom Lake to balance the seasonal temperature needs of the downstream aquatic resources throughout the year. Most outlets at Folsom Dam have or will soon have some type of Temperature Control Device (TCD) to facilitate improved management of cold water in the reservoir. This water is released to control the water temperature in the LAR for the benefit of anadromous fish species downstream of the dam.

The Folsom Lake Raw Water Pump Station (FLRWPS), owned and operated by El Dorado Irrigation District (EID), is located on the south side of the lake, about two miles upstream of Folsom Dam., near El Dorado Hills, California. The FLRWPS provides municipal and industrial (M&I) water to the El Dorado Hills area of El Dorado County. The plant uses submersible pumps inserted in steel casings that extend down the bank of the reservoir.

The current pump operations of FLRWPS utilizing intakes located at lower elevations in the lake reduces the volume of cold water available in the CWP. EID, in collaboration with Reclamation, is proposing to construct a TCD for its water intake facilities at Folsom Lake in order to preserve more of the CWP that can then be used by Reclamation to meet seasonal temperature needs in the LAR.

The purpose of the analysis presented in this technical memorandum (TM) is to assist in the design and construction of the proposed new intake facility with an incorporated TCD. EID desires to incorporate a capability to control the temperature of the water diverted through inclusion of a TCD in the design of the intake. The TCD would provide EID the ability to withdraw water from Folsom Lake at varying depths, thereby minimizing cold water extraction from the reservoir. The TCD would minimize the negative effects of the EID diversion on the Folsom Lake CWP by withdrawing warmer water through the intake.

The TM is designed to address subtasks 1A and 2A of Cooperative Agreement 05FC201041 between Reclamation and EID by studying the feasibility of alternative configurations as they relate to economic attractiveness and environment management. The goal of this TM is to find the appropriate balance between capital costs and environmental benefits.

Folsom Lake Cold Water Pool

Folsom Lake is characterized by a seasonal temperature stratification process such that during the winter and early spring, the temperature in the lake is uniformly cold at all elevations due to low ambient air temperatures and the high volume spring inflow of very cold snowmelt water. During the summer, a warmer upper layer referred to as the "epilimnion" forms as cold water inflows decrease and the upper

surface water of the lake warms due to higher ambient air temperatures and increased solar radiation. The warm water tends to “float” on the colder water deeper in the lake. This colder, lower layer is referred to as the “hypolimnion”. Between these two layers, a thin layer called the “thermocline” forms, which is a region of rapid temperature change between the epilimnion and the hypolimnion. The elevation of the thermocline declines over the summer as the epilimnion increases.

The CWP at Folsom Lake is described as all water in the lake at or below approximately 60°F. This value has been generally accepted by Reclamation as it represents an approximate upper limit to the release temperature from Folsom Lake that protects downstream aquatic resources in the LAR during the critical fall time period. The temperature also typically falls near the thermocline region of Folsom Lake when it is stratified and is therefore an indicator of the temperature stratification of the lake. Reclamation operates Folsom Dam and Nimbus Dam to maintain daily average water temperatures that does not exceed 65°F in the LAR at Watt Avenue from June 1 through October 15 for juvenile steelhead over-summer rearing. Reclamation assumes 5°F of warming as water moves downstream, so a 65°F Watt Avenue temperature requires 60°F water released from Folsom Dam. This temperature is referred to as the target temperature and annual temperature targets have varied between 60°F and 64°F for the period of record used in the analysis presented in this TM. Annual temperature targets for releases at Folsom Dam were as follows: 2002-62°F, 2003-60°F, 2004-64°F, 2005-60°F, 2006-60°F, 2007-63°F, and 2008-64°F.

Temperature Control Device

A TCD operates by allowing control of the elevation, and therefore the temperature, of the water diversion. An intake with a single low level intake maintains no ability to control the temperature of water and may access cold water during the spring and summer and warm water late in the summer and fall as the surface elevation falls and the epilimnion becomes thicker. Adding additional intake levels and/or reducing the required minimum hydraulic head required for pumps improve the intake performance in regard to cold water extraction by allowing access to the warmer water earlier in the year, thereby protecting the CWP for Reclamation use.

While no TCD structure can eliminate all potential effects to the Folsom Lake CWP from future diversion, incorporating a TCD on the FLRWPS with multiple intake elevations provides the opportunity to greatly reduce impacts from future EID diversions. The configurations evaluated in this analysis indicate that a TCD with a minimum or base intake elevation at 320 feet msl, combined with intakes clustered at higher levels provides significant benefits to conservation of the CWP.

Analytical Methods

An Excel-based tool was developed to perform the analysis of the TCD. The number of intakes proposed for the TCD, the minimum head requirement, and an annual temperature target between 60°F and 64 °F are all parameters that can be specified in the tool. The Excel-based tool represents a comparative assessment for evaluation of multiple TCD configuration scenarios. The numbers in the report are not derived from hydraulic or temperature modeling and do not represent absolute volume of water or temperature results. The model does not take into consideration operation and maintenance considerations, costs, recreation, aesthetics, and physical design constraints and is purely a numerical analysis. A tutorial including assumptions, operations, and input requirements used by the Excel-based tool are presented as an addendum to this Technical Memorandum.

For an intake to function there is a minimum head that must be present above the intake based on hydraulic considerations. As long as this pump head requirement is met, individual intake elevations are only required to provide adequate head to allow sufficient flow into the intake structure to meet the

pumping rate. Two hydraulic head values were considered, consisting of 10-foot and 15-foot hydraulic head.

The model then selects the location of the intake elevations based on the operation of the TCD for the 2002 through 2008 period using EID projected water demands, Folsom Lake temperature profiles provided by Reclamation, and historical annual target temperatures provided by Reclamation for each of those years. Due to the large number of potential TCD configuration, a VBA macro was developed in the Excel model that analyzes all potential combinations of intake elevations for diversions. The possible combinations of TCD intake elevations for a given number of intake elevations are evaluated and the macro cycles through each of the combinations, and selects the sets of intake elevations that yield the largest May-October and annual average diversion greater than the target temperature. May-October is the time of year is when the TCD is anticipated to provide CWP to Folsom Lake.

The temperature data used in the model is based on Folsom Lake temperature profiles from 2002 to 2008 provided by Reclamation. The water temperature at 5-foot intervals between 300 feet msl and the lake surface and the temperature profile for each day in the period of record was estimated from each temperature profile using linear interpolation. EID furnished existing water demand, future water demand at year 2013 (when the TCD is anticipated to be operational), and at full build-out, year 2030 for the FLRWPS. The existing demand calculation is based on the average pumping from the years 2004 to 2008. The future pumping assumes an annual total of 13,000 acre-feet (af) for year 2013 and 28,700 af for year 2030 using demand magnitude distributed on the same monthly pattern as the existing level water demand.

Summary

For this analysis, the assumption is made that all water that is diverted with a temperature greater than the target temperature (60°F to 64°F) does not negatively affect the CWP, or conversely that water diverted with a temperature of less than the target temperature may negatively affect the CWP.

The results of the TCD analysis are presented in Tables 1 through 12, which show existing water demands, year 2013 water demands, and year 2030 water demands. The tables compare the results of the existing condition intake configuration and the one-, two-, three-, and four-intake configurations, using a 10-foot and 15-foot minimum intake head requirement. The model output tables also show percent of water diverted from the CWP as well as elevations on all outputs showing adit elevations with maximum benefit to the CWP.

The first column, “ $\geq$ Target Diverted”, represents the water diverted at a temperature greater than the target temperature ranked by TCD performance. The second column, “ $\geq$ Target Missed”, represents the water diverted at less than the target temperature because of limited number of intake elevations (due to the elevation of the TCD intake). The third column, “ $\geq$ Target Unavailable”, represents the water diverted at less than target temperature because of limitation based on minimum hydraulic head requirements. The fourth column, “No Water $\geq$ Target”, represents the volume of water diverted when no water greater than the target temperature was available in the reservoir. The fifth column, “ $<$ Target Diverted”, provides the sum of columns two through four representing the total amount of water less than target temperature diverted whether due to facility constraints or environmental conditions.

Cold water diverted as a result of intake location or minimum head requirements can be minimized by careful placement and design considerations of the intakes and/or incorporation of additional intake elevations in the TCD. These considerations allow the TCD to better follow the elevation between the top of the CWP and the minimum head requirement to protect the CWP.

This implies that the design configuration of the TCD impacts its effectiveness in two main ways:

- Minimum hydraulic head requirement – Defines how early in the year warm water can be accessed to protect the CWP.
- Number and elevation of intakes – Defines how well the TCD can follow the minimum hydraulic head requirement.

As shown in the tables, all proposed TCD configurations provide improved operational capability compared to existing conditions. Based on the analysis, a significant reduction of the CWP diversion is realized by utilization of the TCD for all water demand scenarios. Costs were not included in this evaluation, however cost trade-offs will occur in reducing the minimum required hydraulic head and adding additional intake elevations. The optimal configurations appear to include the minimum intake elevation with the other intake elevations clustered at the higher elevations. This implies that the minimum intake elevation should be designed to be used in many years and not just as an emergency intake for years with extremely low Folsom storage levels.

Notes on tables:

1. Number of intakes represents base intake at 320 feet msl plus additional intakes above the base intake elevation.
2. Target Missed: Water diverted at less than the target temperature because of a limitation in number of intakes.
3. Target Unavailable: Water diverted at less than the target temperature because of the minimum hydraulic head requirement.
4. All water in lake less than target temperature.

Addendum: El Dorado Irrigation District Temperature Control Device Model Tutorial

1.0 Introduction

This tutorial is intended to provide information for use by EID in the design and implementation of a new intake with a Temperature Control Device (TCD) to meet projected future demands. The attached CD containing the TCD Model should be accompanied by this tutorial at all times to explain its use. The analysis represents an evaluation of the effectiveness of potential TCD configurations under consideration in protection of the Folsom Lake Cold Water Pool (CWP). The spreadsheet tool used in this evaluation represents a comparative assessment for evaluation of multiple TCD configuration scenarios based on interpolation of current available data from EID and Reclamation. The numbers in the report are not derived from hydraulic or temperature modeling and do not represent absolute volume of water or temperature results.

2.0 Potential TCD Operation

For this analysis, the assumption is made that all water that is diverted at an elevation with a temperature greater than the target diversion temperature (60°F to 64°F) does not negatively affect the CWP, or conversely that water diverted with a temperature of less than the target diversion temperature may negatively affect the CWP.

For an intake at any elevation to function, there is a minimum head that must be present above the intake based on hydraulic considerations. With the pumps at a fixed elevation at the lower end of the intake, there would be a minimum head requirement for operation of the pumps that would not vary. As long as this pump head requirement is met, individual intake elevations would only require adequate head to allow sufficient flow into the intake structure to meet the pumping rate. This minimum head has a potentially large impact on the effectiveness of the TCD. This implies that the design configuration of the TCD impacts its effectiveness in two main ways:

- Minimum hydraulic head requirement – Defines how early in the year warm water can be accessed to protect the CWP.
- Number and elevation of intakes – Defines how well the TCD can follow the minimum hydraulic head requirement.

3.0 Evaluation Tool

An Excel-based tool was developed to perform the analysis of the TCD performance. The user can enter the desired minimum head requirement, an annual target diversion temperature between 60°F and 64 °F, and the number of the intakes proposed for the TCD. The tool models the operation of the TCD for the historical 2002 through 2008 period using EID current and projected future water demands.

The Excel-based tool operates such that for each day of data:

1. Estimate the hydraulic head limit as the surface elevation minus the user input minimum head requirement. Check that the water surface elevation is above the required minimum elevation for the intake structure. This verifies that the intake structure is physically capable of a diversion that day.

2. Estimate the water temperature at this elevation.
3. Select the highest available outlet elevation.
4. Estimate the water temperature at this elevation.
5. Select the highest usable intake elevation based on the surface elevation and the minimum required head for that intake elevation.
6. Obtain the water temperature at that intake elevation.
7. Classify the diversion according to the water temperatures as:
 - a. If surface temp < target temperature, diversion goes into None Avail > target temperature (60°F to 64°F) and into Diversion < target temperature (60°F to 64°F)
 - b. If head limit temp < target temperature (60°F to 64°F), diversion goes into Unavail > target temperature (60°F to 64°F) and into Div < target temperature (60°F to 64°F).
 - c. If intake elevation temp < target temperature (60°F to 64°F), diversion goes into Missed > target temperature (60°F to 64°F) and into Div < target temperature (60°F to 64°F)
 - d. Goes into Div > target temperature (60°F to 64°F)
8. Save the set of intake elevations that produce the highest volume of water greater than the target temperature for each intake configuration.
9. Develop a revised output summary to support the new analysis.
10. The evaluation criteria used will be to maximize the volume of water diverted above the target temperature to minimize the effect on the CWP from the EID diversion

The Excel workbook contains a worksheet for each TCD alternative configuration. Each of these sheets can accept input of annual diversion target temperature and the minimum hydraulic head. The VBA macro that analyzes all potential combinations of intake elevations under the design assumptions cycles through each of the combinations, saves the results of each evaluation, and selects the set of intake elevations that yield the largest year-by-year annual average and May-October Div > target temperature, in addition to the all year average. The results for each year are summarized in both tabular and graphical formats, on individual worksheets and on the summary sheet. The results of the evaluation are summarized in tabular and graphical formats. **Figure 1** is an example of the graphical output. The elevation of each intake can also be manually entered, which allows alternative configurations that may be necessary for operational constraints to be quantitatively compared to the modeling optimization.

The line plots in the upper portion of the graphic include the water surface elevation, the maximum hydraulic limit on intake elevation, the top of the CWP (target temperature), and the intake used in the day. The colored area plots at the bottom of the figure represent the results of the analysis. The green represents the water diverted at a temperature > target temperature implying the more green the better the TCD performed. All other colors represent water diverted at < target temperature.

The red area represents the water diverted at < target temperature because of the minimum hydraulic head requirement, the bright blue (missed) represents the water diverted at < target temperature because of the limited number of intake elevations, and the light blue represents the water diverted at < target temperature because there was no water > target temperature in Folsom Lake. This gives a visual representation of the performance of the TCD and the potential for improvements.

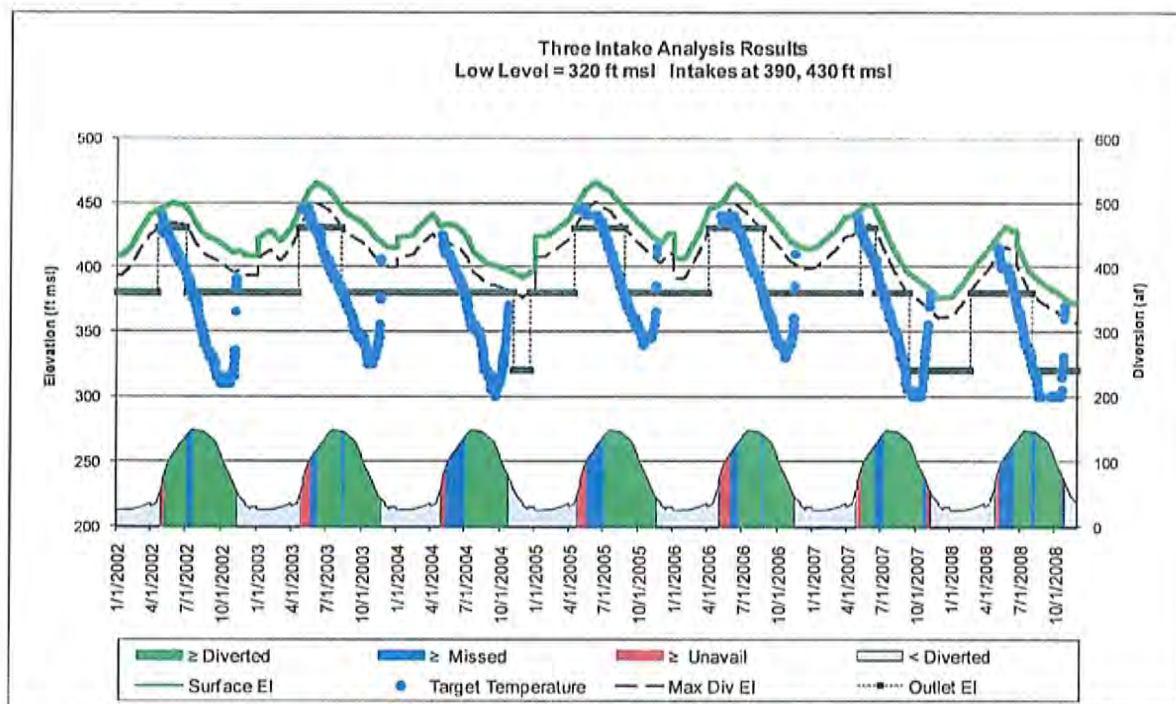


Figure 1 - Example Output for an Alternative Evaluation, with annual target temperature.

There are a large number of potential TCD configurations. A VBA macro was developed in the Excel tool that analyzes all potential combinations of intake elevations under the design assumptions. All possible combinations of TCD intake elevations for the given number of intake elevations are listed on the appropriate worksheets. The macro cycles through each of the combinations, saves the results of each evaluation, selects the sets of intake elevations that yield the largest all year and annual average May-October Div > target temperature. The results are summarized in both tabular and graphical formats.

An additional VBA macro was then developed to cycle through the different number of intake elevation worksheets, and the potential minimum hydraulic head values. This macro sets the minimum hydraulic head then calls the appropriate macro to compute the “optimal” set of intake elevations for the current worksheet. The “optimal” results are then copied to the worksheet “Summary” where they are stored and used to produce graphical and tabular summaries of the entire analysis. This macro can be executed by clicking the button in the “Summary” worksheet.

4.0 TCD Analysis Assumptions

Constant:

- Assume the 2002 through 2008 period is adequate to represent the potential range of operation of Folsom Lake for selection of the number and elevation of the intakes for the TCD since this is the entire period of record available for this data. This data set covers essentially the entire range of reservoir conditions through dry to wet years.
- Assume a low-level intake at 320-foot elevation mean sea level (msl) for use in extreme surface drawdown years to ensure adequate hydraulic head for operation of the intake in all alternatives.

This intake could also be utilized during winter when water is not available with no impact to the CWP.

- Assume that each intake elevation has sufficient flow capacity to handle the entire anticipated diversion rate. EID's goal for the TCD is to divert the warmest water possible to protect the CWP while minimizing raw water treatment costs and odor and taste concerns of treated water.

Vary by Alternative:

- For each minimum hydraulic head, assume an alternative with an intake every 5 feet from 330 to 440 feet msl elevation. This alternative is an attempt to eliminate the "lost" diversion to give an estimate of a theoretical best TCD configuration at each minimum hydraulic head.
- Assume a minimum Folsom Reservoir surface elevation of 350 feet msl for use of the intake structure. The reservoir elevation data included in the analysis tool never goes below 366 feet msl during the analysis period and this minimum does not constrain the current analysis. The elevation was included in the tool to provide opportunity for future design changes, if necessary.
- Assume a minimum required head for use at each intake elevation. Two minimum head values, 10 and 15 feet were used to explore the sensitivity of the TCD performance to this variable. Final minimum head submergence will be determined during the design process.
- Assume the maximum intake elevation for the TCD is 440 feet msl. This assumption adds a number of additional potential intake elevation combinations to each configuration.

4.1 Temperature Data Development

The basic temperature data is the historical Folsom Lake water temperature profiles from 2002 to 2008. Linear interpolation was used to estimate the water temperature at 5-foot intervals between the 300 foot msl elevation and the surface elevation at each profile date. Linear interpolation was then used between dates to get an estimated water temperature profile for each day of the period of record. There is a time period between the late fall and early spring in each year, when the temperature data is not available due to lack of profile data. This does not affect the analysis as there is little or no stratification of Folsom Lake during this time period and the water temperatures are always below the 60°F target.

4.2 EID Diversion Data

EID furnished both existing and projected future water demand data for the FLRWPS as shown in Table 1. The existing data is based on the historical pumping from 2004 to 2008. The 2030 "buildout" demand assumes an annual total water demand of 28,700 acre-feet (af) distributed on the same magnitude and monthly pattern as the existing level water demand. The data was converted to daily values by simply taking a daily running average of the data for each day of the month. The resulting daily values were then summed by month and compared to the original monthly data to verify that the total monthly volume was maintained. **Figure 2** shows the comparison. **Figure 3** shows the original monthly data and the monthly total data from the new daily data. This process results in a set of daily values with two potential considerations:

- The daily peak diversion matches the mean monthly peak diversion
- The monthly totals computed from the daily flows do not exactly match the initial monthly diversion totals.

These two issues are both relatively small and within the limits of other assumptions in the analysis. The final computed volumes in each category are intended for comparative use as an indicator of TCD effectiveness and not as absolute volumes. Since these values will be the same in all alternatives they are assumed to not have a substantial impact on the comparative analysis.

Table 1 - Estimated EID Diversion at FLRWPS

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total
	(acre-feet)												
Existing	241	226	297	367	861	1075	1289	1272	1086	770	428	280	8191
2030	843	793	1040	1285	3017	3768	4516	4456	3805	2697	1499	982	28700

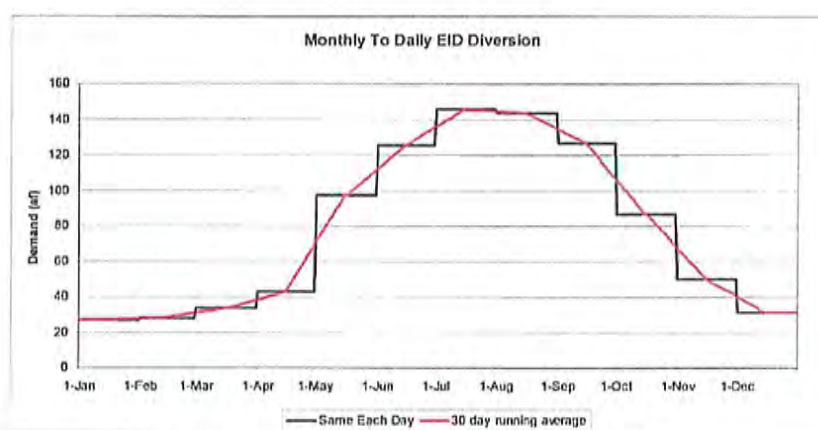


Figure 2 - Monthly to Daily EID Diversion at FLRWPS

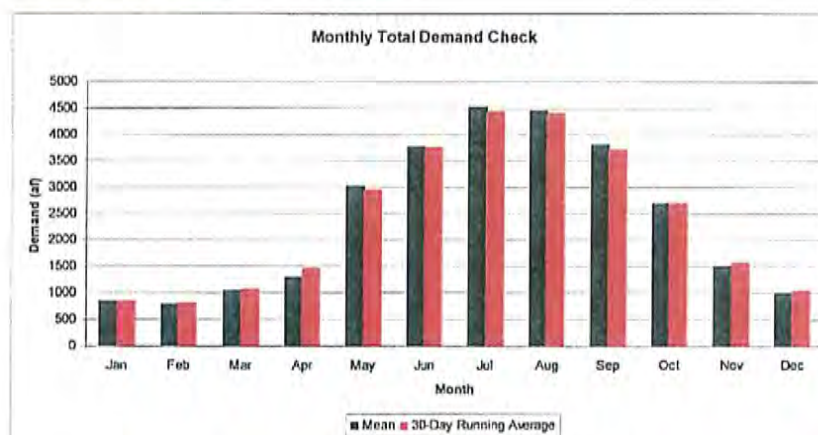


Figure3 - Monthly Total Demand Check

An additional worksheet was included in the workbook to evaluate the existing EID diversion under the same rules as the potential TCD configurations to represent existing and potential future demands without a TCD in place. The existing level monthly diversion data furnished by EID was converted to daily

diversion values using the same process as used with the future level data. The existing intake was configured with two intake elevations at 330 and 350 feet msl elevation. These were assumed to operate with up to 1/3 of the maximum daily diversion diverted through the 350 foot msl intake if hydraulically available.

Comparison of Alternative Intake Configurations
 Potential Impact to Folsom CWP - Best 2002 Configuration
 Minimum Intake Head = 15 ft

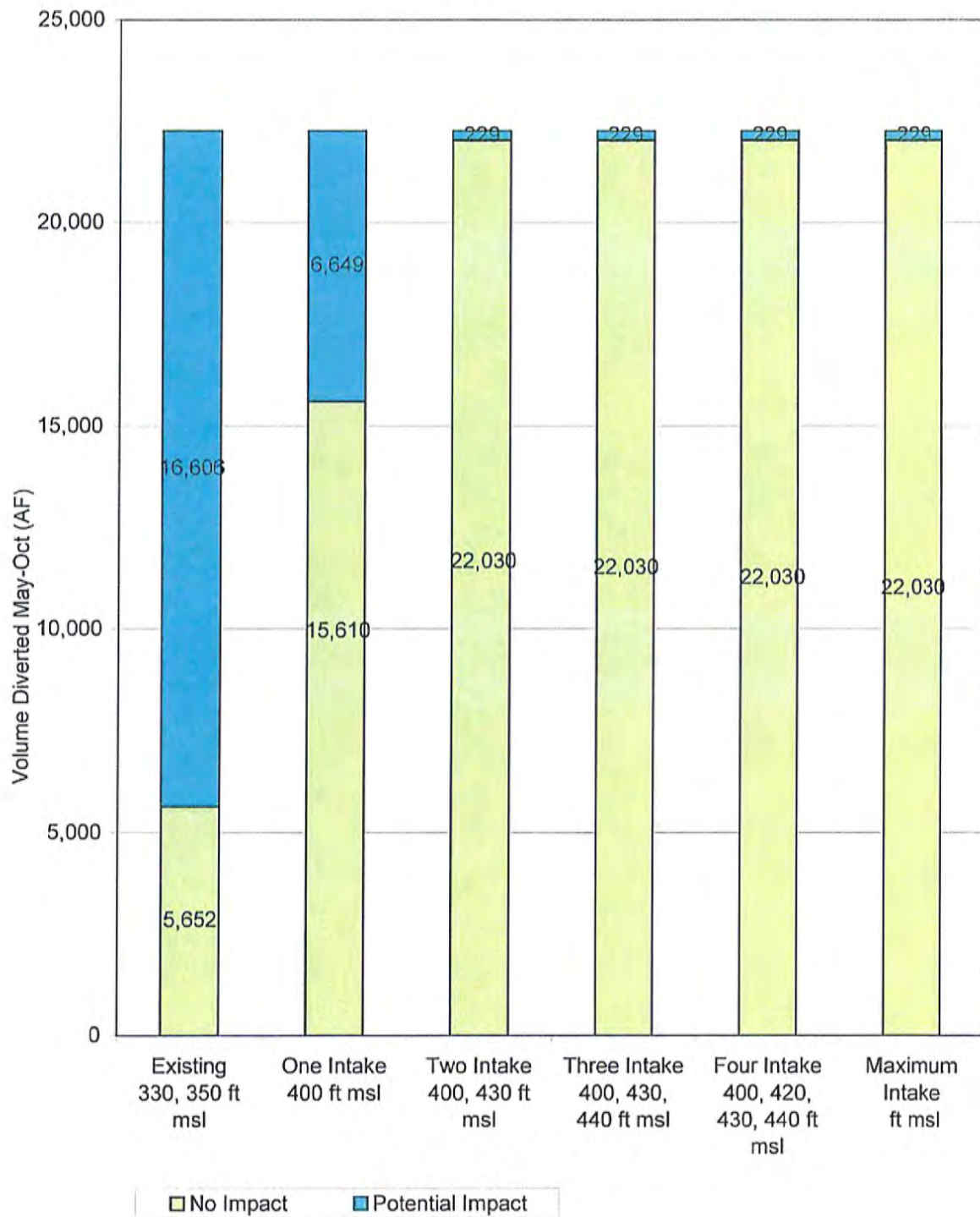


Figure 1

Comparison of Alternative Intake Configurations
 Potential Impact to Folsom CWP - Best 2003 Configuration
 Minimum Intake Head = 15 ft

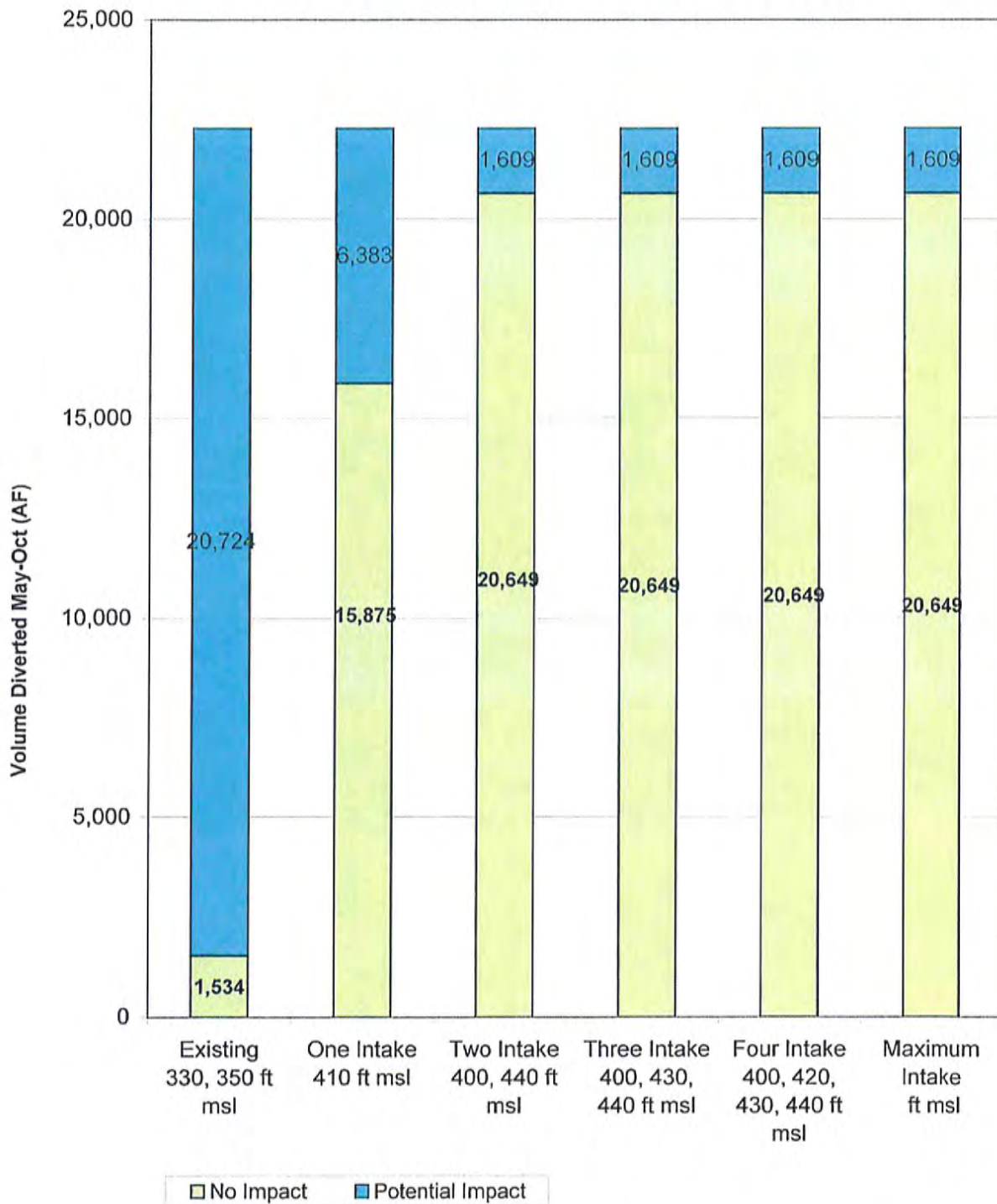


Figure 2

Comparison of Alternative Intake Configurations
 Potential Impact to Folsom CWP - Best 2004 Configuration
 Minimum Intake Head = 15 ft

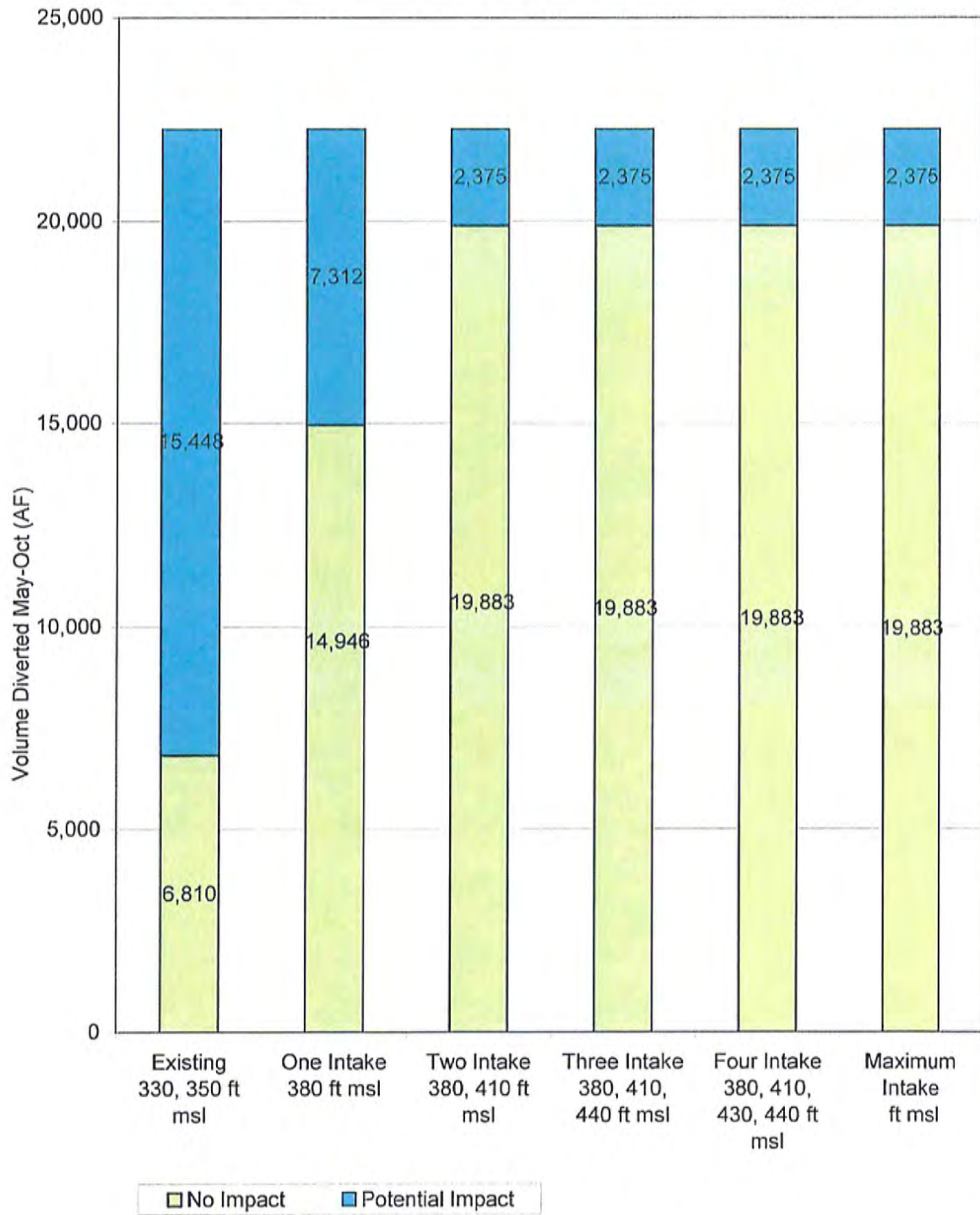


Figure 3

Comparison of Alternative Intake Configurations
 Potential Impact to Folsom CWP - Best 2005 Configuration
 Minimum Intake Head = 15 ft

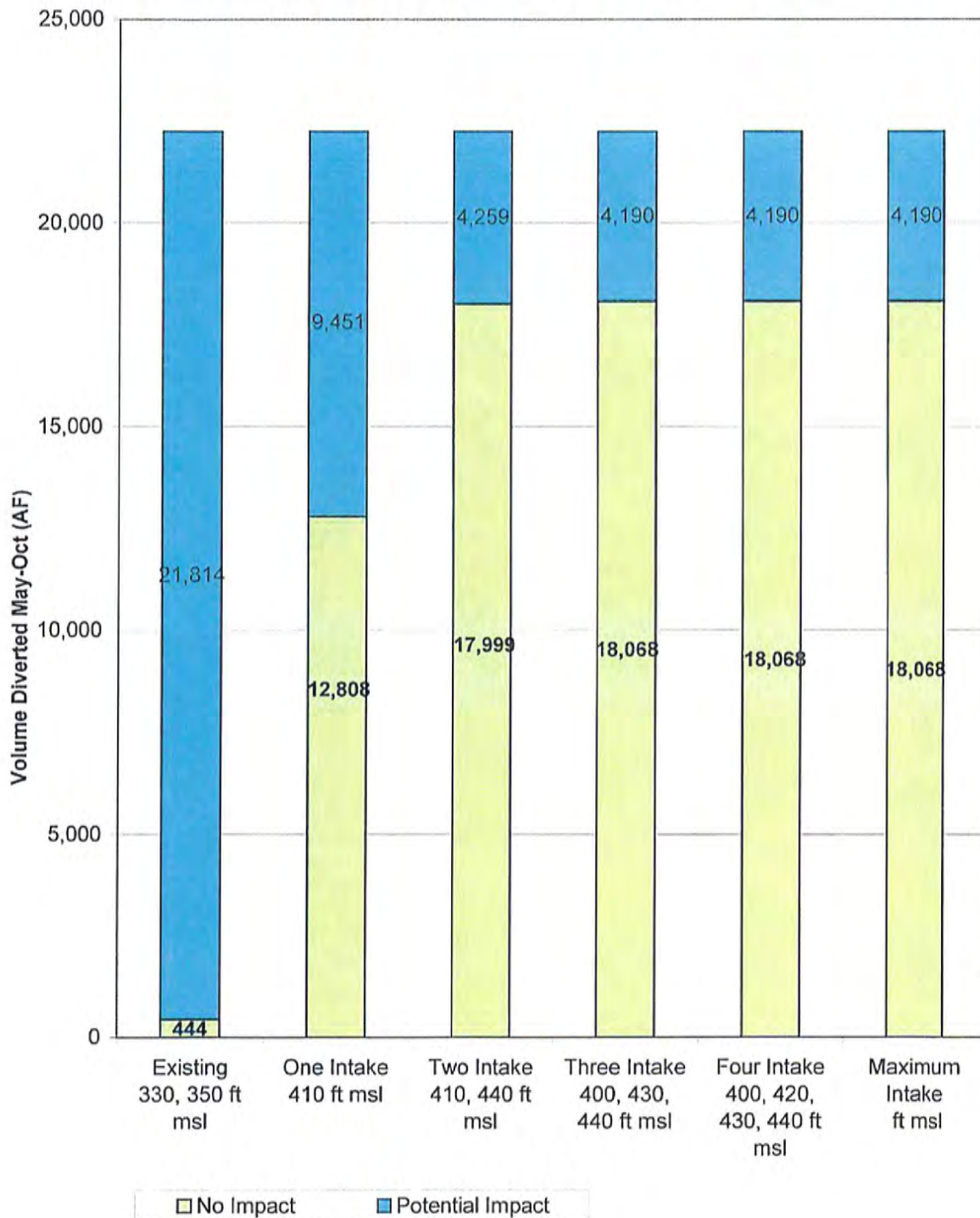


Figure 4

Comparison of Alternative Intake Configurations
 Potential Impact to Folsom CWP - Best 2006 Configuration
 Minimum Intake Head = 15 ft

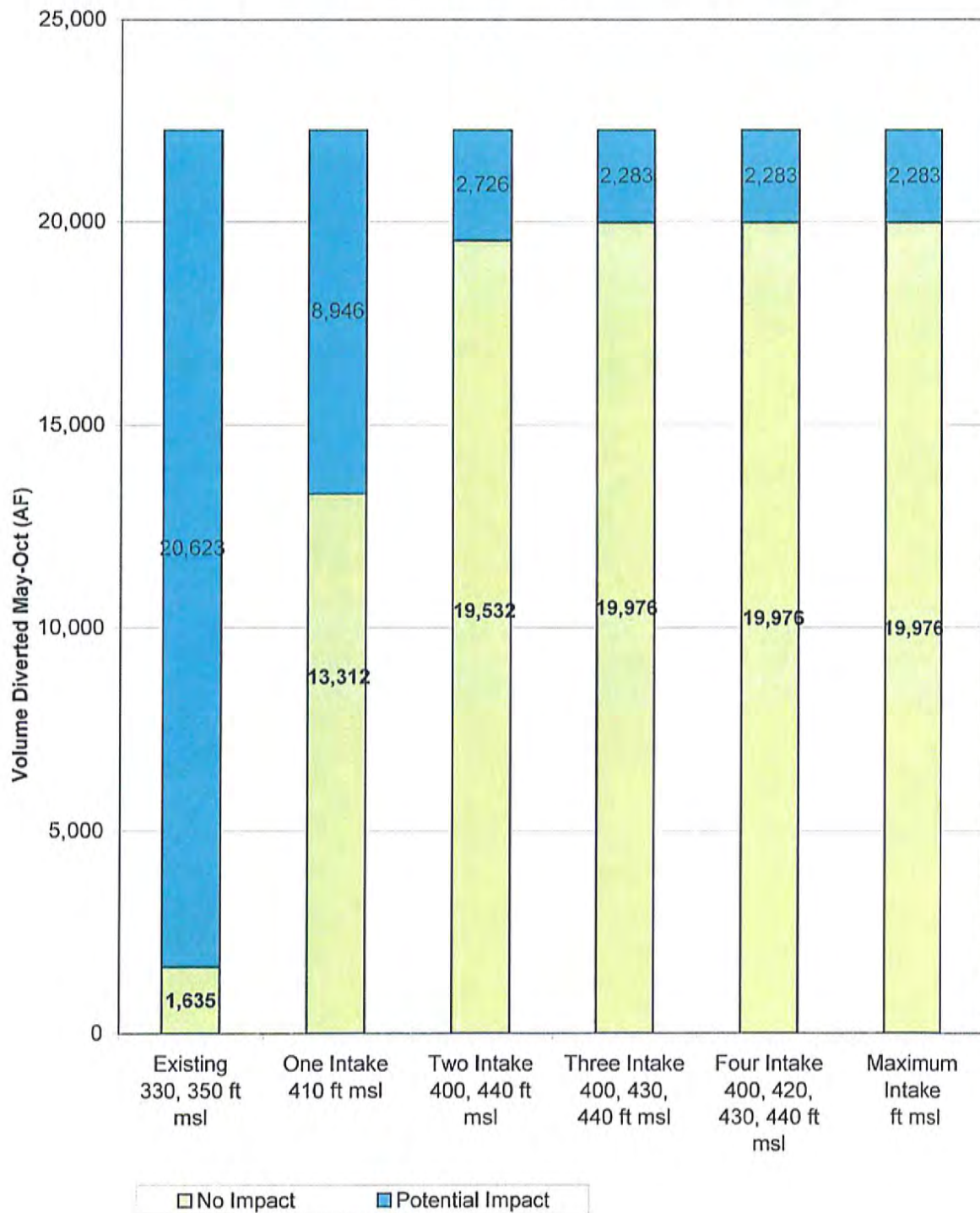


Figure 5

Comparison of Alternative Intake Configurations
 Potential Impact to Folsom CWP - Best 2007 Configuration
 Minimum Intake Head = 15 ft

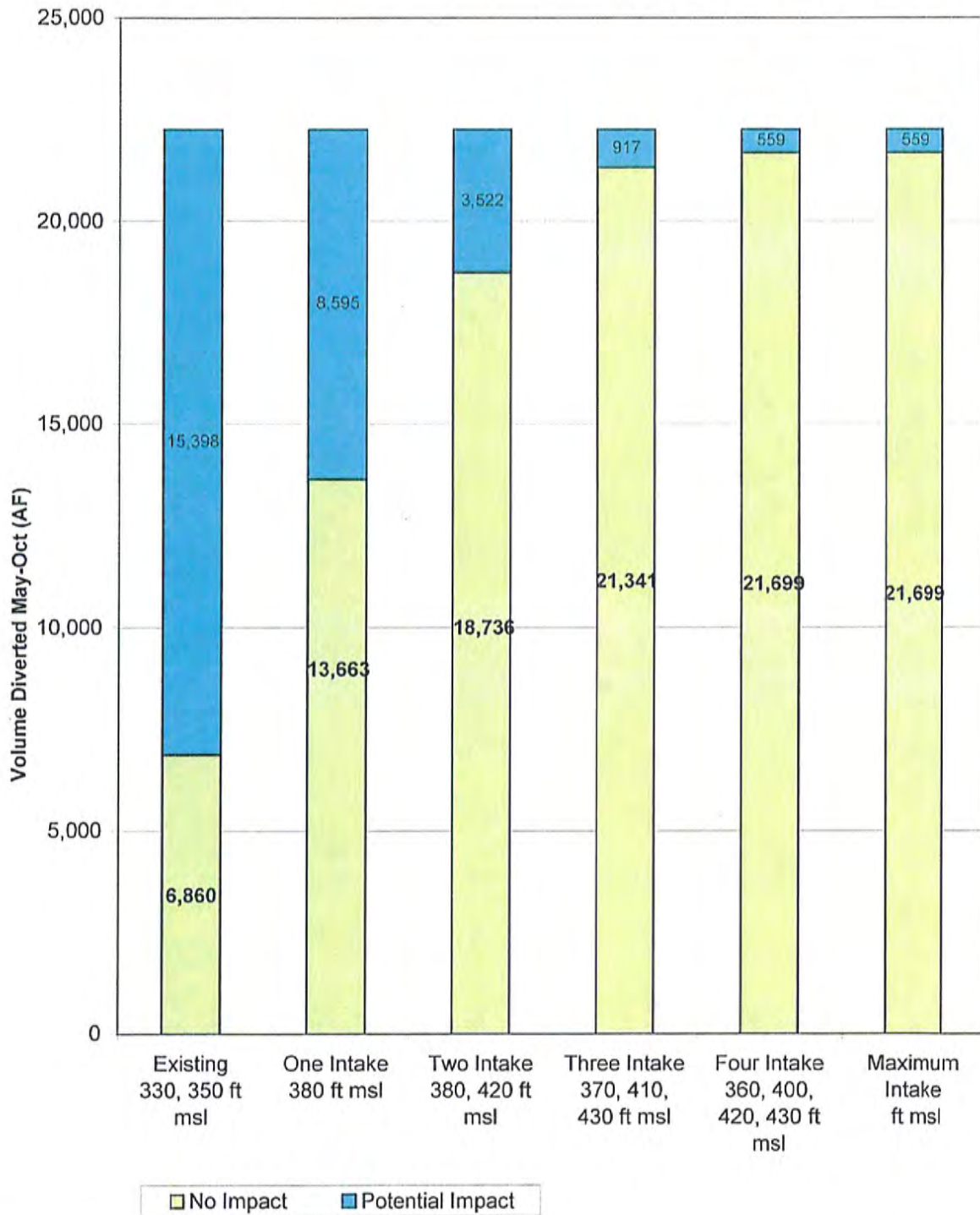


Figure 6

Comparison of Alternative Intake Configurations
 Potential Impact to Folsom CWP - Best 2008 Configuration
 Minimum Intake Head = 15 ft

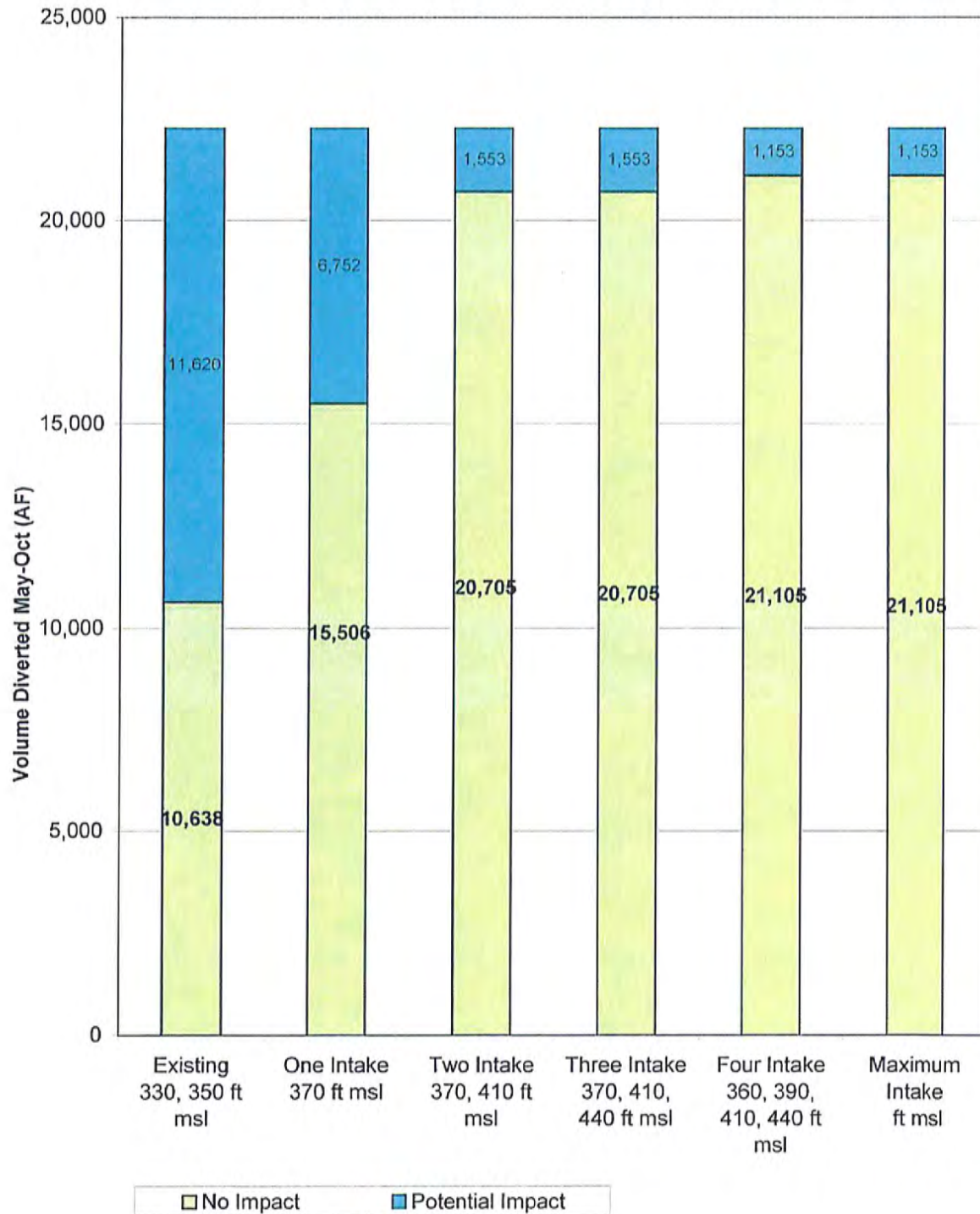


Figure 7

Comparison of Alternative Intake Configurations
 Potential Impact to Folsom CWP - Best Average Configuration
 Minimum Intake Head = 15 ft

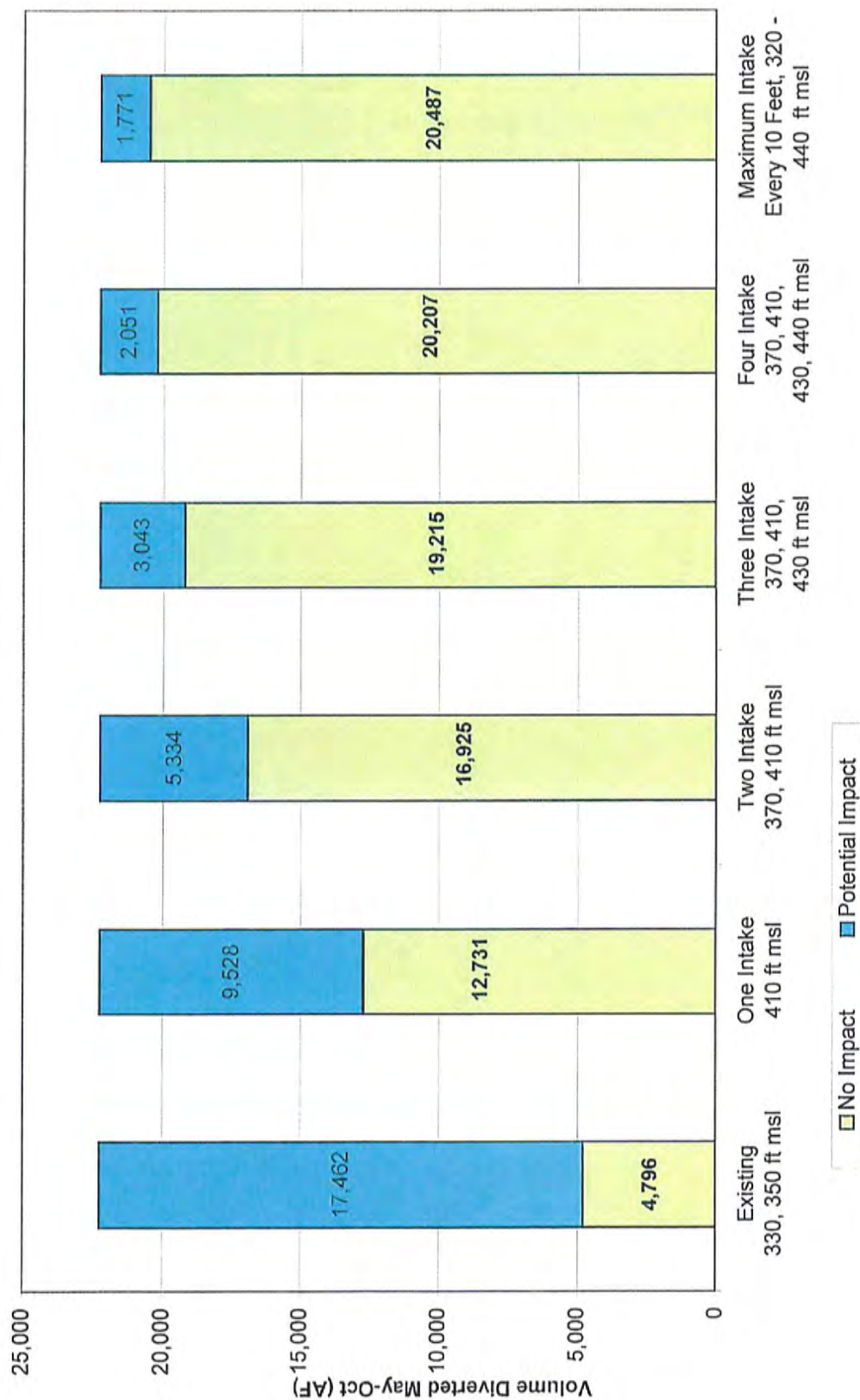


Figure 8

Table 1.

Comparison of Alternative Intake Configurations: Potential Impact to Foliom CWP

Minimum Intake Head - 10
Existing Demand 8,193 AF

(units = AF)

[illegible]

Table 2

Comparison of Alternative Intake Configurations Potential Impact to Folsom CWP

Maximum Initial Head = 10
Existing Demand 2,193 AF

(CIVITS = %)

[illegible]

6. 1772

Comparison of Alternative Intake Configurations

Potential Impact to Folsom CWP

CI = probability of infection

NOT PREPARED

$$Ch_{n+1} = AF$$
[illegible]

Copy

Comparison of Alternative Intake Configurations Potential Impact to Folsom CWP

Editorial Board

82 pages

(Chairs = %)

[illegible]

